

# **Numerical Simulation of Coupled Multiphase Fluid Flow and Mechanics for Gas Migration in Bentonite Considering Heterogeneous Distributions**

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# **1. Introduction**

The final disposal method for high-level waste is Deep Geological Disposal. By the principles of isolation and retardation, the waste decays harmlessly, isolating it from the biosphere and ensuring human health and environmental safety.

However, after hundreds of years of disposal, gas may be generated due to the corrosion of metallic materials under anoxic conditions, radioactive decay of waste, or the radiolysis of water. As gas degrades the barrier's capability, endangering the safety of the repository. Thus, buffer materials play a crucial role in the repository





Buffer materials (Bentonite)



Collect experimental data

2. Flow chart

bentonite is commonly chosen as the buffer materials. In practical situations, bentonite exhibits different particle arrangements, porosity, and permeability, presenting heterogeneous distributions.

Therefore, this study utilized gas injection laboratory experiment data and applied the THMC7.1 numerical model to simulate gas migration, aiming to better understand gas pressure accumulation. Additionally, it investigated the impact of heterogeneous bentonite on gas flow.

# **3. Experimental data**

Gas injection experiments were conducted in the laboratory by the British Geological Survey (Daniels et al., 2017). This experiment spanned 121 days and was divided into three phases: 1.Hydration (0-39d) 2.Gas injection (39-71d) 3.Gas turned-off (71-121d).





#### 6. Results & Discussion

**Results** 

THMC7.1 (Thermal-Hydrology-GeoMechanics-Reactive Chemical Transport Model) is a 3-D finite element model of fully coupled four processes.



Thermal transport (T) Multiphase fluid flow (H) Geo-mechanics (M) Chemical transport (C)

Thermal Hydrology Geo-Mechanics Reactive Chemical Model

#### Multiphase fluid flow (H) module N

• Mass conservation equation:

$$\frac{\partial \rho_{\alpha} \phi S_{\alpha}}{\partial t} + \nabla \cdot (\rho_{\alpha} V_{\alpha}) + \nabla \cdot (\rho_{\alpha} \phi S_{\alpha} V_{s}) = M^{\alpha}, \alpha \in \{L\}$$
  
in which  $V_{\alpha} = -\frac{k_{r\alpha} k}{\mu_{\alpha}} \cdot (\nabla P_{\alpha} + \rho_{\alpha} g \nabla z) \quad V_{s} = \frac{du}{dt}$ 

• Capillary pressure / Relative permeability / Saturation law: (Parker et al., 1987)

$$\begin{cases} \tilde{S}_{t\alpha} = 1 & \text{if } P_{C\alpha+1,\alpha} \leq 0 \\ \tilde{S}_{t\alpha} = \left[ 1 + \left( \bar{\alpha} P_{C\alpha+1,\alpha} \right)^N \right]^{-M} & \text{if } P_{C\alpha+1,\alpha} > 0 \end{cases}, \alpha \in \{ L, \alpha \} \\ \tilde{S}_{t\alpha} = \left[ 1 + \left( \bar{\alpha} P_{C\alpha+1,\alpha} \right)^N \right]^{-M} & \text{if } P_{C\alpha+1,\alpha} > 0 \end{cases}$$

### **Geo-mechanics (M) module**

• Mass conservation equation:

$$\frac{\partial \rho_s \phi_s}{\partial t} + \nabla \cdot (\rho_s \phi_s V_s) = 0$$

• Momentum balance equation:

t: the time (T)  $\rho_{\alpha}$ : the density of  $\alpha$ -th fluid phase (ML<sup>-3</sup>)  $\phi$ : the porosity (-)  $S_{\alpha}$ : the normalized saturation of  $\alpha$ -th fluid phase (-)  $\alpha$ : the Darcy velocity of  $\alpha$ -th fluid phase (LT<sup>-1</sup>) s: the velocity of the solid  $(LT^{-1})$  $M^{\alpha}$ : the sum of the artificial source/sink rate of all species in  $\alpha$ -th fluid phase (ML<sup>-3</sup>T<sup>-1</sup>)

 $k_{r\alpha}$ : the relative permeability of i-th fluid (-) **k**: the permeability of porous medium (L<sup>2</sup>)  $\mu_{\alpha}$ : the viscosity of  $\alpha$ -th fluid (ML<sup>-1</sup>T<sup>-1</sup>)  $P_{\alpha}$ : the pressure of the  $\alpha$ -th fluid phase (ML<sup>-1</sup>T<sup>-2</sup>) g: the gravitational acceleration (LT<sup>-2</sup>) **z**: the potential head (L) **u**: the displacement of the media (L)

 $T^{-2}$ )

, 
$$\alpha \in \{L - 1\}$$
;  $\tilde{S}_{tL} = 1$   
 $\tilde{S}_{t\alpha}$ : the accumulated saturation of  $\alpha$ -th fluid phase (-)  
 $P_C$ : the capillary pressure (ML<sup>-1</sup>T<sup>-2</sup>)  
 $\bar{\alpha}$ : the scaling factor related to the entry pressure (ML<sup>-1</sup>  
 $N$  and  $M$ : the curve shape parameter (-)  $M=1-1/N$ 

 $\rho_s$ : the density of solid (ML<sup>-3</sup>)  $\phi_s$ : the porosity of solid (-) **T**: the Cauchy stress tensor ( $ML^{-1}T^{-2}$ )

 $P_s$ : the pressure of solid (ML<sup>-1</sup>T<sup>-2</sup>)  $S_1, S_2$ : the elastic parameters (ML<sup>-2</sup>T<sup>-2</sup>)  $\lambda, \mu_1, \mu_2, \mu_3$ : the viscous parameters (ML<sup>-1</sup>T<sup>-1</sup>)

The initial gas saturation is 0.01. However, as gas is injected over time, the gas pressure increases, and the gas saturation gradually rises.



Fig. 7. The modelling result of gas pressure **Fig. 8.** The modelling result of gas saturation **Fig. 9.** The modelling result of gas velocity(z)

## **Results considering the heterogeneous distributions**

Dividing into two distributions of bentonite.



Fig. 11. The heterogeneous distributions of bentonite



$$-\nabla \cdot \mathbf{T} + \sum_{\alpha \in \{L\}} \nabla \left( S_{\alpha} P_{\alpha} \right) - \left[ \sum_{\alpha \in \{L\}} \rho_{\alpha} \phi S_{\alpha} + \rho_{s} \phi_{s} \right] \boldsymbol{g} \nabla \mathbf{z} = -\phi_{s} \rho_{s} \frac{d^{2} \boldsymbol{u}}{dt^{2}} \approx 0$$

• Constitutive law for viscous-elastic material:

$$\mathbf{T} = -\phi_s P_s \mathbf{I} + S_1 \mathbf{B} + S_2 \mathbf{B}^{-1} + \lambda (tr \mathbf{D})\mathbf{I} + 2\mu_1 \mathbf{D} + \mu_2 (\mathbf{D}\mathbf{B} + \mathbf{B}\mathbf{D}) + \mu_3 (\mathbf{D}\mathbf{B}^{-1} + \mathbf{B}^{-1}\mathbf{D})$$
  
in which  $\mathbf{B} = \mathbf{F}\mathbf{F}^T$ ,  $\mathbf{F} = \mathbf{I} + \mathbf{H}$ ,  $\mathbf{H} = \nabla \mathbf{u}$ ,  $\mathbf{D} = \frac{1}{2} (\dot{\mathbf{H}} + \dot{\mathbf{H}}^T)$ ,  $\dot{\mathbf{H}} = \nabla \dot{\mathbf{u}} = \nabla V_s$ 

#### **Coupled H-M analysis**





# **7.** Conclusions

This study successfully simulated the migration behavior of water and gas two-phase fluids in bentonite using the THMC7.1 numerical model. Considering the heterogeneity of bentonite, the modelling results of gas velocity reveal that gas preferentially migrates to areas with high porosity and high permeability. This finding is significant for the design and safety assessment of deep geological disposal facilities.

### 8. References

- Daniels, K.A., Harrington, J.F., "The Response of Compact Bentonite during a 1D Gas Flow Test" British Geological Survey Open Report, OR/17/067, 22pp, 2017.
- Parker, J.C., Lenhard, R.J., Kuppusam, T.Y., "A parametric model for constitutive properties governing multiphase flow in porous media" Water Resoures., 23, 618-624, doi: 10.1029/WR023i004p00618, 1987.